

# AN11066

SDARS active antenna 1st stage LNA with BFU730F, 2.33 GHz

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Application note

## Document information

Info	Content
<b>Keywords</b>	LNA, 2.33 GHz, BFU730F, SDARS.
<b>Abstract</b>	This document provides circuit, layout, BOM and performance information for 2.33 GHz LNA equipped with NXP Semiconductors BFU730F wide-band transistor.



## Revision history

Rev	Date	Description
v.1	20111025	Initial version

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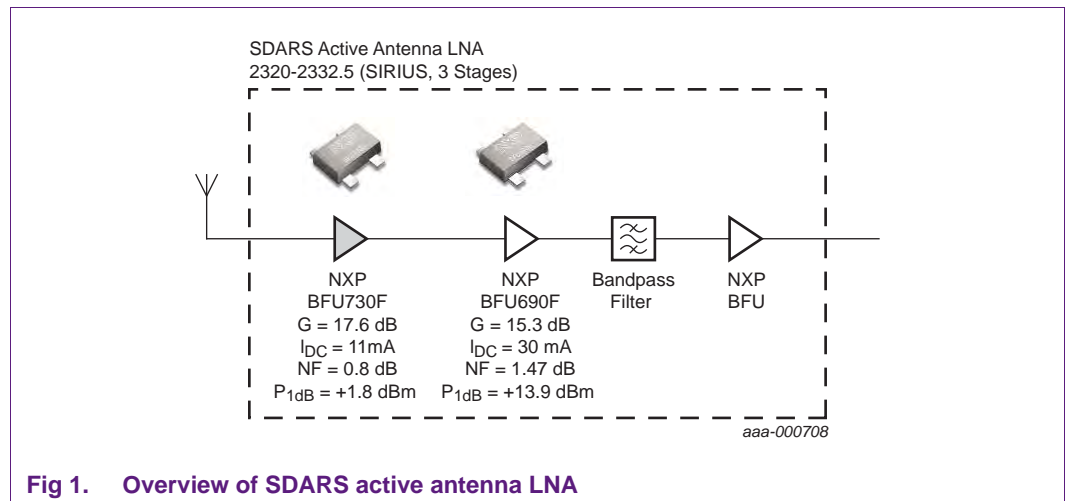
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## 1. Introduction

The BFU730F is a wideband Silicon Germanium Amplifier transistor for high speed, low noise applications. It is used for LNA applications such as GPS, satellite radio, cordless phone and wireless LAN. The BFU730F comes in a SOT343F package that contains two emitter pins for improved grounding.

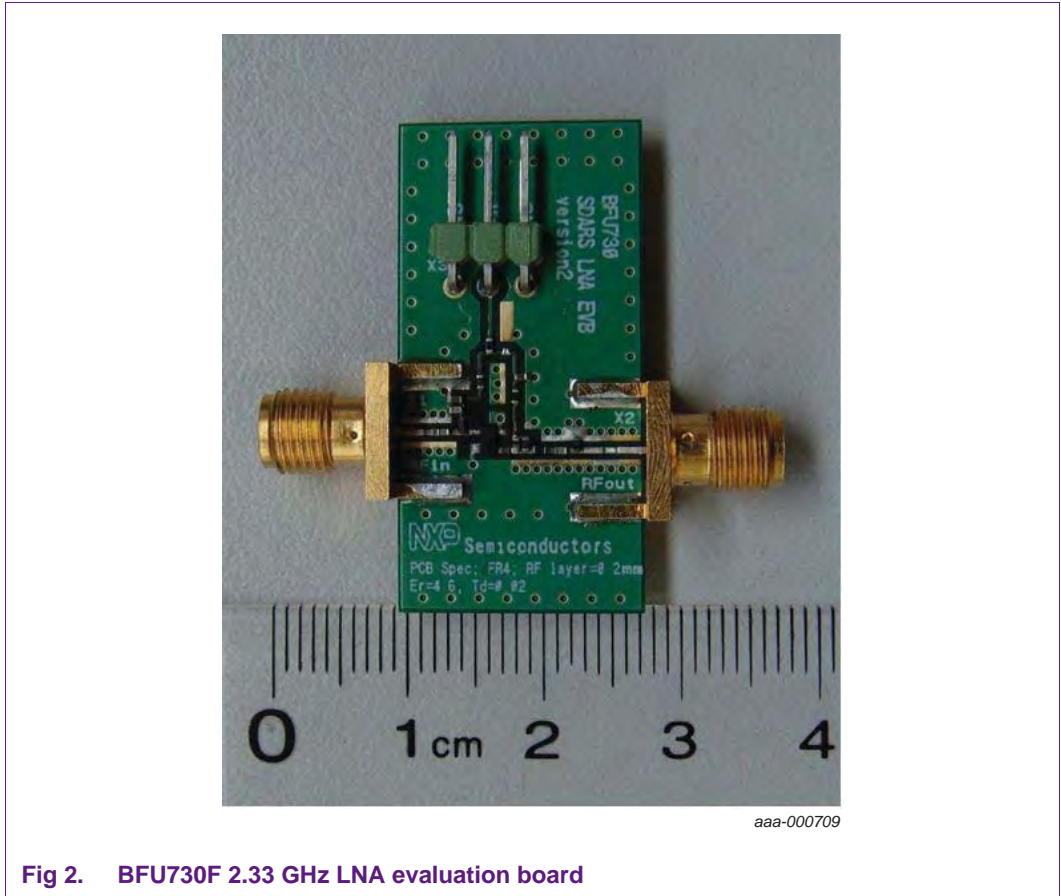
The BFU730F is ideal in all kinds of application where cost matters. It also provides the designer with increased flexibility.

BFU730F SiGeC low noise transistor is shown in [Figure 1](#) in a Satellite Digital Audio Radio Service (SDARS) active antenna LNA application. It is intended for use as the first stage in a three stage SIRIUS LNA chain.



The 2.33 GHz LNA evaluation board (EVB) is designed to evaluate the performance of the BFU730F transistor applied as the first stage in a three stage SIRIUS LNA chain. This document provides an application diagram, board layout, bill of material, and some typical results.

[Figure 2](#) depicts the evaluation board.



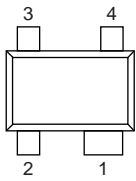
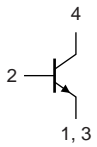
## 2. General description

The BFU730F is a discrete HBT produced in NXP Semiconductors SiGeC QuBIC4x BiCmos process. SiGeC is in principle a normal silicon germanium process with the addition of Carbon in the base layer of the NPN transistor. The presence of carbon in the base layer suppresses the boron diffusion during wafer processing. This process allows steeper and narrower SiGe HBT base and a heavier doped base. This results in lower base resistance, lower noise and higher cut-off frequency (higher gain). [Table 1](#) provides a summary of the transistor performance in terms of noise and gain is shown.

**Table 1. BFU730F values, measured at, 2 V,  $V_{ce}$  and 5 mA IC**

Frequency (GHz)	Noise (dB)	Associated gain (dB)
1.5	0.50	25
1.8	0.50	23.5
2.4	0.55	21.5
5.8	0.80	15.0
12	1.30	11.0

**Table 2. Pinning information**

Pin	Description	Simplified outline	Graphic symbol
1	emitter		 <i>mbb159</i>
2	base		
3	emitter		
4	collector		

### 3. Application Board

The BFU730F 2.33 GHz EVB simplifies the evaluation of the BFU730F wideband transistor, for this frequency range. The EVB enables testing of the device performance and requires no additional support circuitry. The board is fully assembled with BFU730F, including input and output matching, to optimize the performance. The input match was a compromise between the best noise figure and a low input return loss. The board is mounted with signal input and output SMA connectors for connection to RF test equipment.

#### 3.1 Application Circuit

Figure 3 provides the application diagram as supplied on the evaluation board.

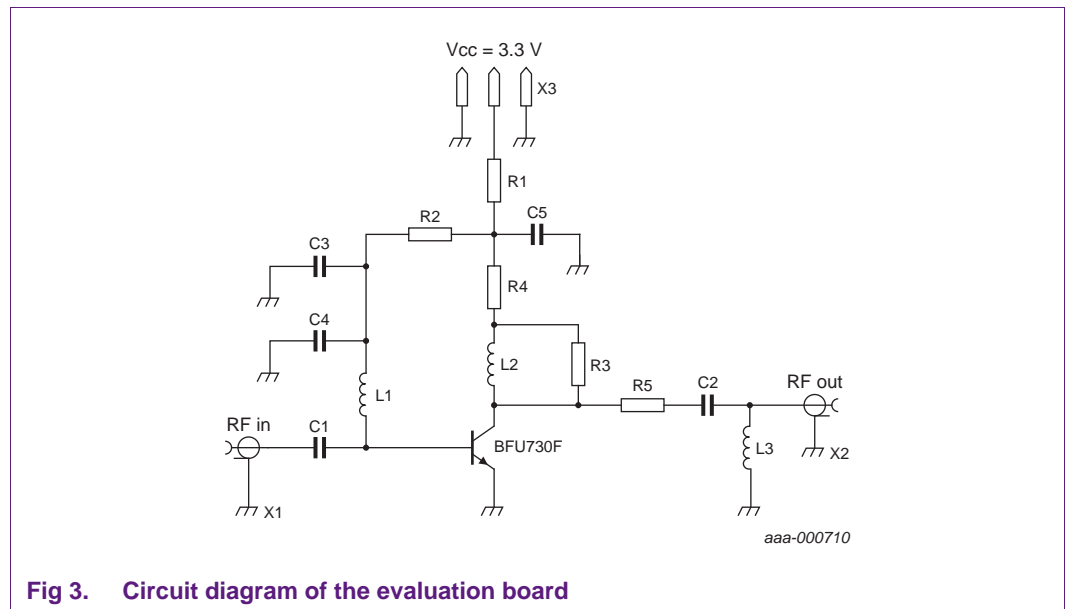


Fig 3. Circuit diagram of the evaluation board

### 3.2 Board Layout

Figure 3 shows the board layout including components.

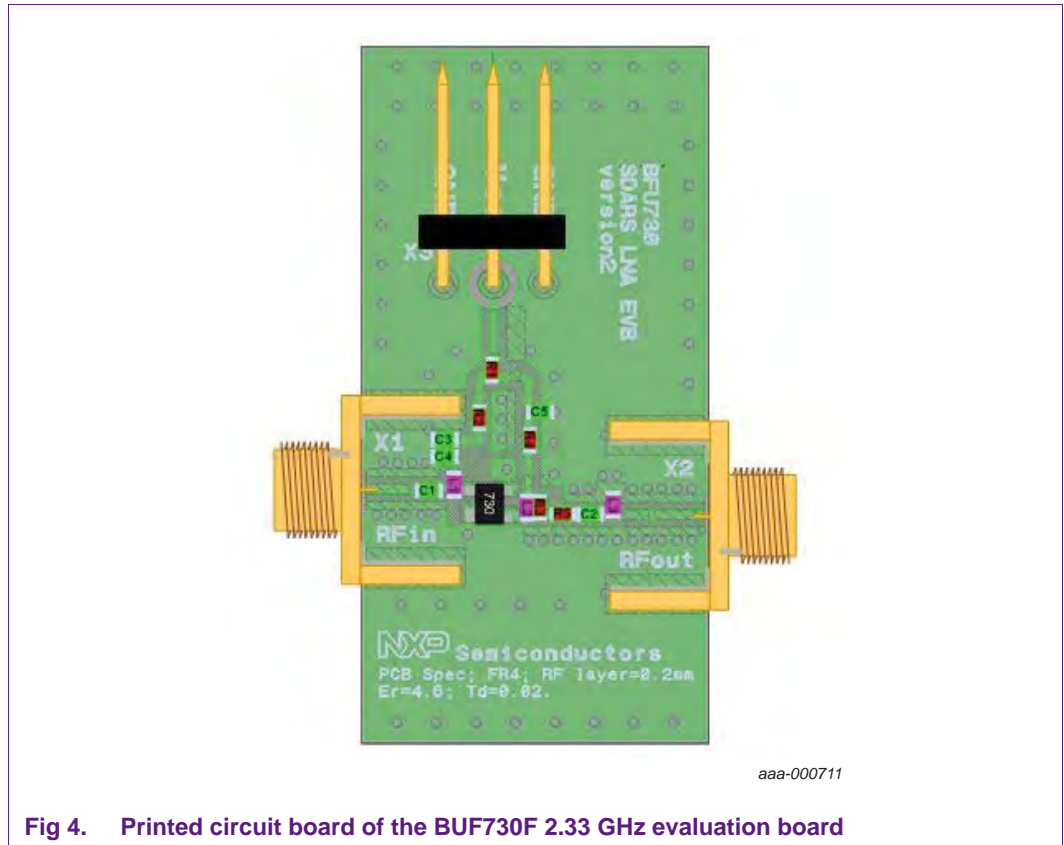


Fig 4. Printed circuit board of the BFU730F 2.33 GHz evaluation board

### 3.3 PCB layout

A good PCB Layout is an essential part of an RF circuit design. The EVB of the BFU730F serves as a guideline for laying out a board using the BFU730F. Use controlled impedance lines for all high frequency inputs and outputs. Bypass  $V_{CC}$  with decoupling capacitors, preferable located as close as possible to the device. For long bias lines, it may be necessary to add decoupling capacitors in the line further away from the device. Correct grounding of the GND pin is also essential for performance. Either connect the GND pin directly to the ground plane or through vias, or do both.

The EVB is made of FR4 material using the stack shown in Figure 5.

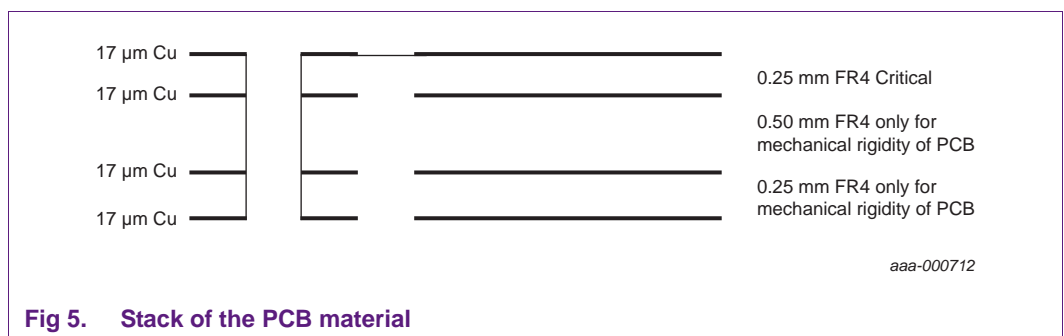


Fig 5. Stack of the PCB material

Material supplier is Isola Duraver;  $\epsilon_r = 4.6$  to 4.9:  $T\delta = 0.02$ .

### 3.4 Bill of materials

**Table 3. Bill of materials**

Designator	Description	Footprint	Value	Supplier name/type	Comment
C1	capacitor	0402	12 pF	Murata GRM1555	input matching/DC blocking
C2	capacitor	0402	3.3 pF	Murata GRM1555	input matching/DC blocking
C3	capacitor	0402	8.2 pF	Murata GRM1555	LF decoupling
C4	capacitor	0402	10 pF	Murata GRM1555	LF decoupling
C5	capacitor	0402	10 pF	Murata GRM1555	LF decoupling
L1	inductor	0402	15 nH	Murata/LQW15A high Q low Rs	input matching/DC bias
L2	inductor	0402	100 nH	Murata/LQW15A	DC bias
L3	inductor	0402	5.8 nH	Murata/LQW15A high Q low Rs	output matching
R1	resistor	0402	130 $\Omega$	various	bias setting temperature stability
R2	resistor	0402	30 $\Omega$	various	bias setting
R3	resistor	0402	100 $\Omega$	various	stability
R4, R5	resistor	0402	0 $\Omega$	various	backup tune pads
X1, X2	SMA RF connector	-	-	Johnson, end launch SMA 142-0701-841	RF input/RF output
X3	DC header	-	-	Molex, PCB header, right angle, 1 row, 3-way 90121-0763	bias connector



## 4. Equipment required

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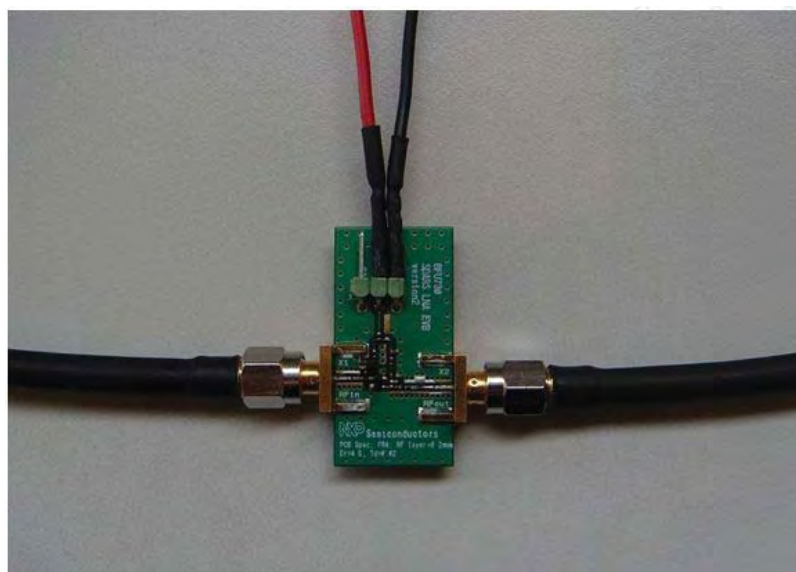
In order to measure the evaluation board the following is required:

- DC power supply up to 30 mA at 3.3 V (up to 15 V for bias control)
- RF signal generator capable of generating an RF signal at the operating frequency of 2.33 GHz.
- RF spectrum analyzer that covers at least the operating frequency of 2.33 GHz as well as a few of the harmonics. A spectrum analyzer that has a noise figure test function which measures up to 8 GHz, is sufficient. This is useful as it eliminates the necessity of having an expensive noise figure analyzer.
- Ammeter to measure the supply current (optional).
- Network analyzer for measuring gain, return loss and reverse Isolation.
- Noise figure analyzer.

## 5. Connections and setup

The BFU730F, 2.33 GHz EVB is fully assembled and tested. The following procedure is a step-by-step guide to operate the EVB and test the device functions.

1. Set the DC power supply to 3.3 V and connect it to the VCC and GND terminals.
2. Connect the RF signal generator and spectrum analyzer to the RF input and the RF output of the EVB, respectively. Do not turn on the RF output of the signal generator yet but set it to  $-30$  dBm output power at 2.33 GHz. Set the spectrum analyzer to 2.33 GHz center frequency with a reference level of 0 dBm.
3. Turn on the DC power supply and it reads approximately 11 mA.
4. Enable the RF output of the generator; the Spectrum analyzer displays a tone of 2.33 GHz at around  $-13$  dBm.
5. A network analyzer (NWA) can be used, instead of a signal generator and spectrum analyzer, to measure gain for input and output return loss
6. To evaluate the noise figure, use either a noise figure analyzer or a spectrum analyzer with noise option. The use of a 15 dB noise source, such as the Agilent 364B, is recommended. When measuring the noise figure of the evaluation board, minimize the use of any kind of adaptors or cables between the noise source and the EVB. Cables and adaptors significantly affect the noise performance.



aaa-000713

Fig 6. Printed circuit board of the BUF730F 2.33 GHz evaluation board

## 6. Typical EVB Results

Table 4. Typical measurement results measured on the evaluation board<sup>[1]</sup>

Symbol	Parameter	value	Unit
NF	noise figure	0.8	dB
$G_p$	power gain	17.6	dB
$RL_{in}$	input return loss	9.4	dB
$RL_{out}$	output return loss	22.5	dB
$\alpha_{isol(r)}$	reverse isolation	29.4	dB
$P_{i(1dB)}$	input 1 dB Gain Compression	-15	dBm
$P_{L(1dB)}$	output 1 dB Gain Compression	1.7	dBm
$IP3_i$	Input third order intercept point	4.7	dBm
$IP3_o$	output third order intercept point	22.6	dBm

[1] The NF and gain figures are measured at the SMA connectors of the EVB, so the connectors and PCB losses are not subtracted. When they are subtracted, the NF improves by approximately 0.1 dB.

### 6.1 Noise figure



6.1.1 Noise figure tabular data

Table 5. Frequency list results<sup>[1]</sup>

RF (GHz)	NF (dB)	Noise temperature (K)	Gain (dB)
2.290	0.825	60.701	17.736
2.300	0.827	60.840	17.694
2.310	0.825	60.650	17.662
2.320	0.832	61.259	17.639
2.330	0.822	60.425	17.644
2.340	0.821	60.378	17.641
2.350	0.812	59.642	17.643
2.360	0.834	61.426	17.632
2.370	0.819	60.216	17.609

[1] From Rohde and Schwarz FSU

6.2 Power gain compression test

$V_{CC} = 3.3\text{ V}$  network analyzer is set to CW mode - for example, set to a single frequency, with power sweep. Input power is swept from  $-25\text{ dBm}$  to  $-5\text{ dBm}$  at  $2332.5\text{ MHz}$ . Amplifier reaches input 1 dB compression point ( $P_{i(1dB)}$ ) at  $-15.02\text{ dBm}$  input power. Output  $P_{L(1dB)} = -15.02\text{ dBm} + 16.77\text{ dB gain at } P_{L(1dB)} \text{ point} \geq +1.75\text{ dBm}$ , or  $1.5\text{ mW}$ .

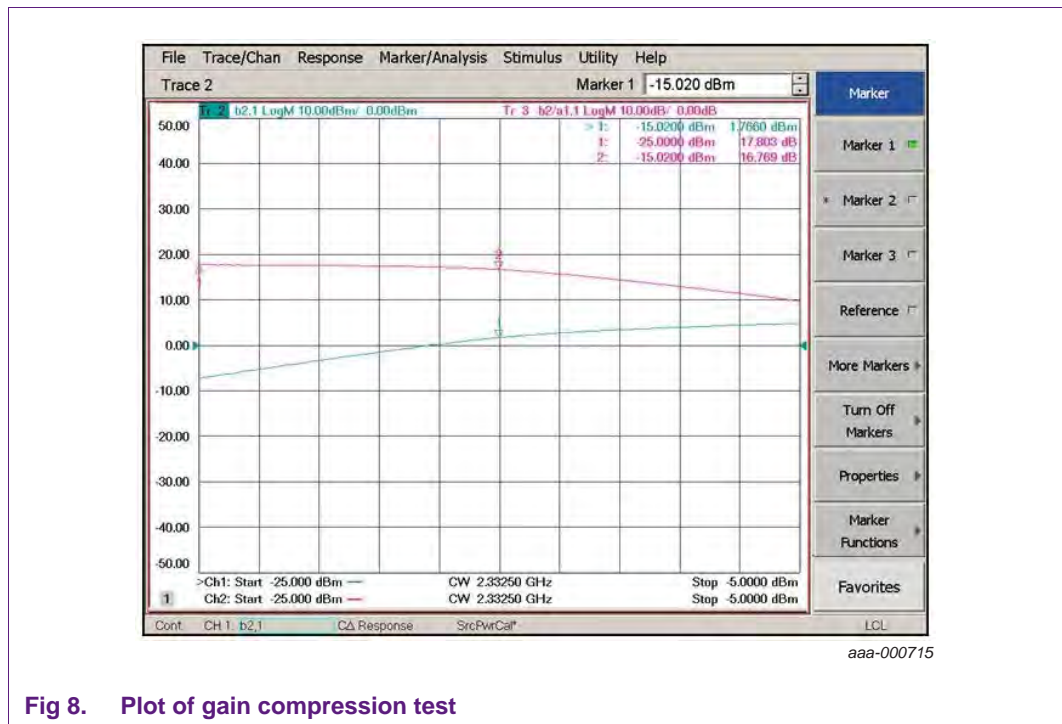


Fig 8. Plot of gain compression test

### 6.3 Input return losses (10 MHz to 6 GHz)

#### 6.3.1 Log Mag

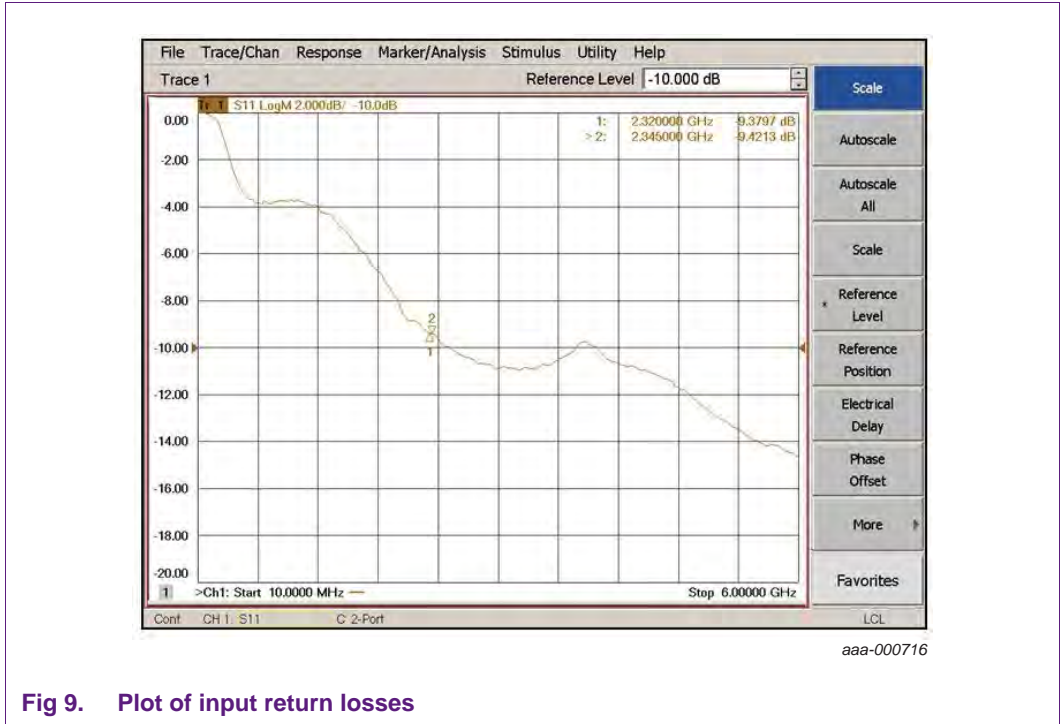
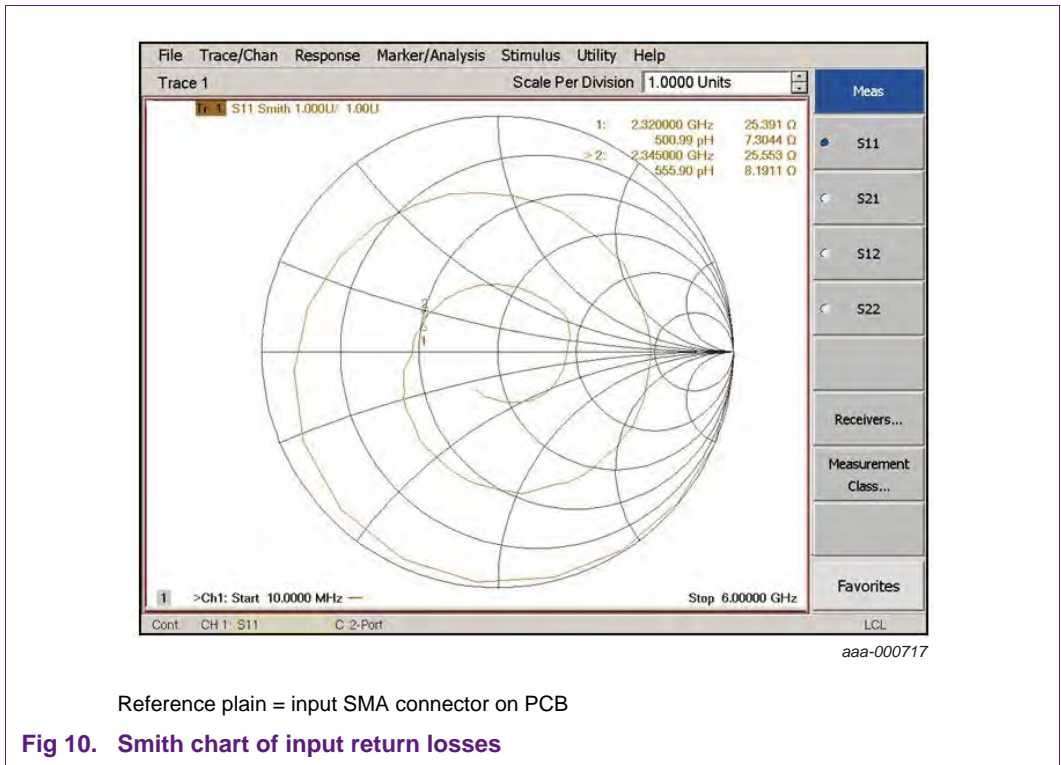


Fig 9. Plot of input return losses

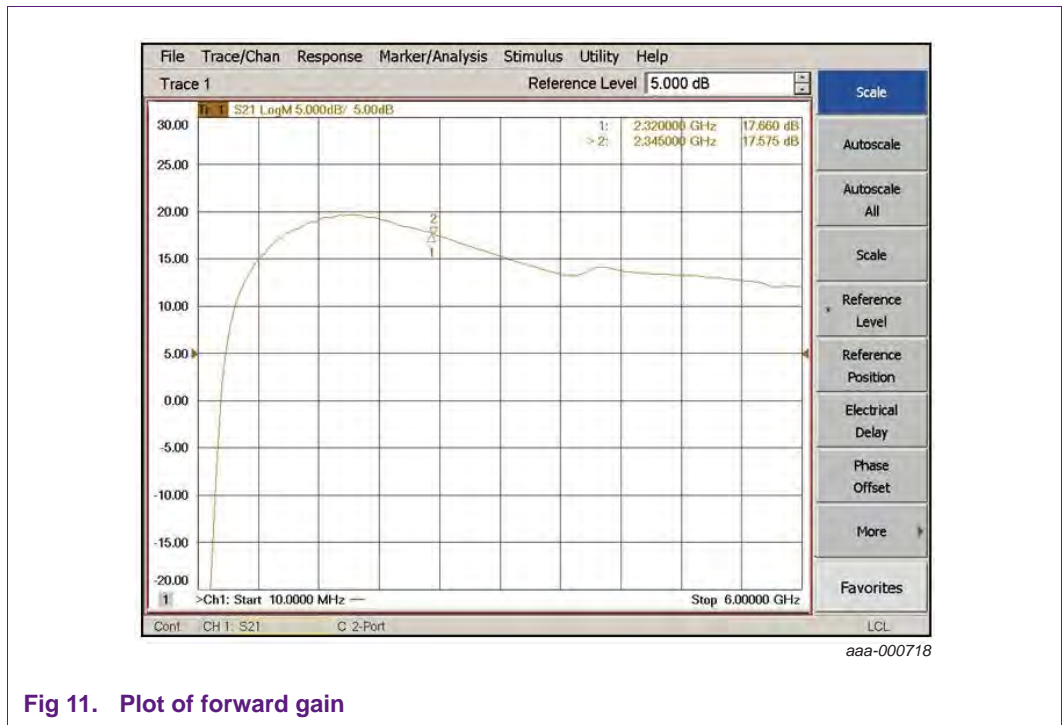
#### 6.3.2 Smith chart



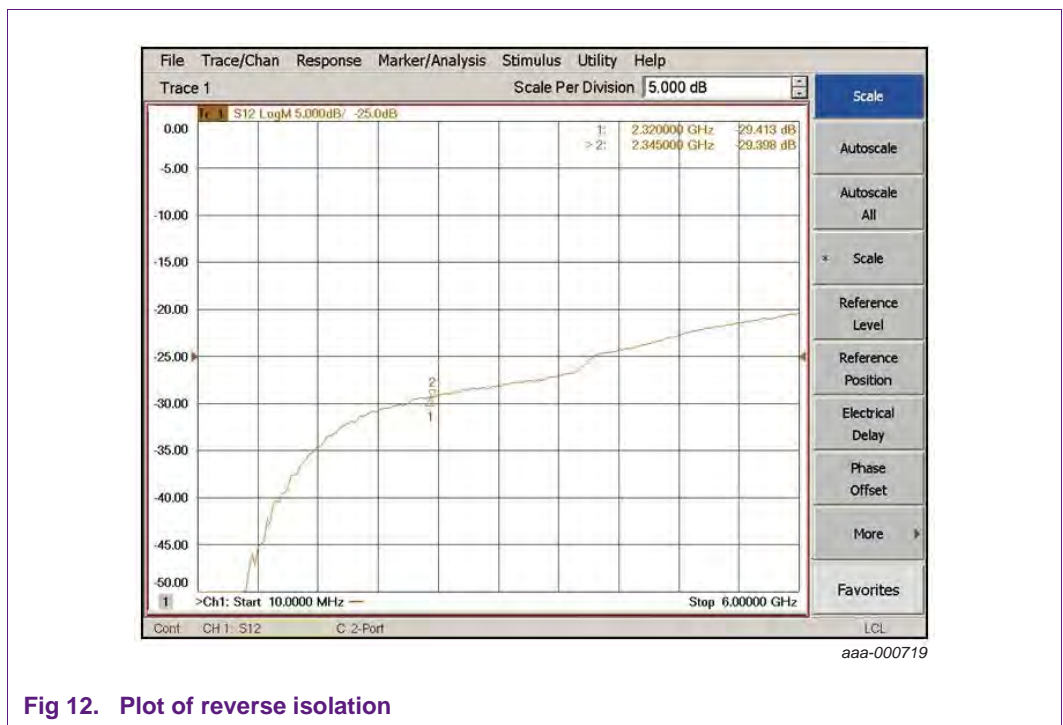
Reference plain = input SMA connector on PCB

Fig 10. Smith chart of input return losses

### 6.3.3 Forward gain - wide sweep



### 6.4 Reverse isolation

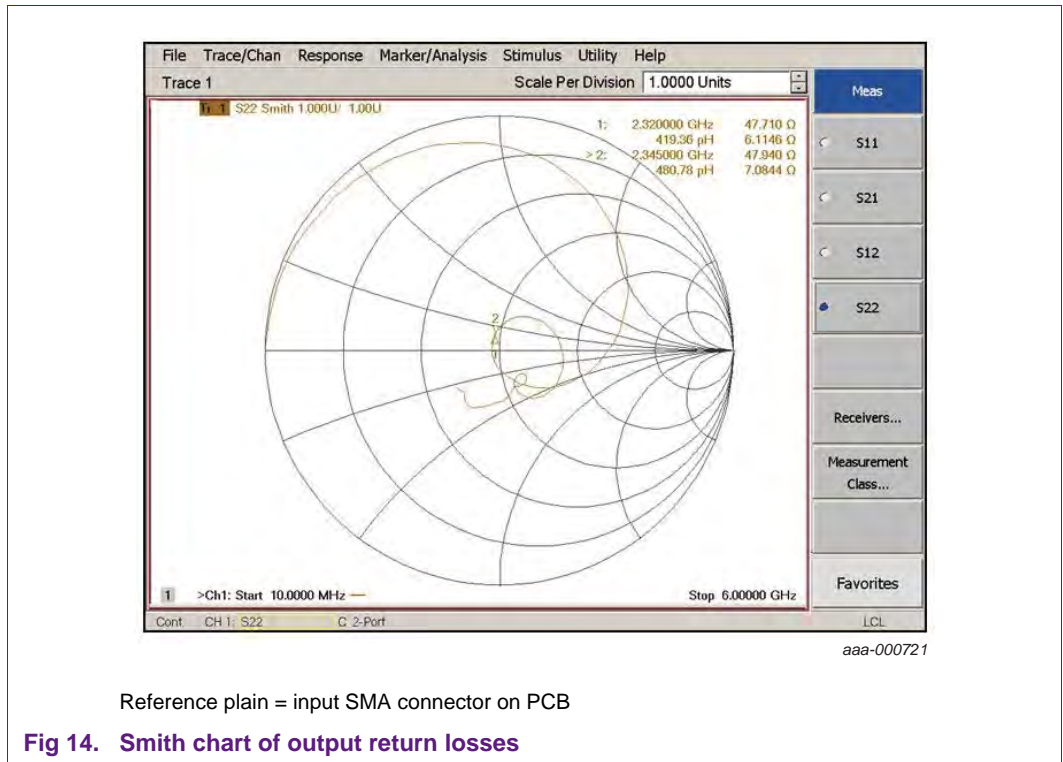


### 6.5 Output return losses (10 MHz to 6 GHz)

#### 6.5.1 Log Mag



#### 6.5.2 Smith chart



6.6 Two-tone test (2332 MHz)

6.6.1 Input stimulus for amplifier two-tone test

- $f_1 = 2332$  MHz
- $f_2 = 2333$  MHz
- $-24.37$  dBm for each tone

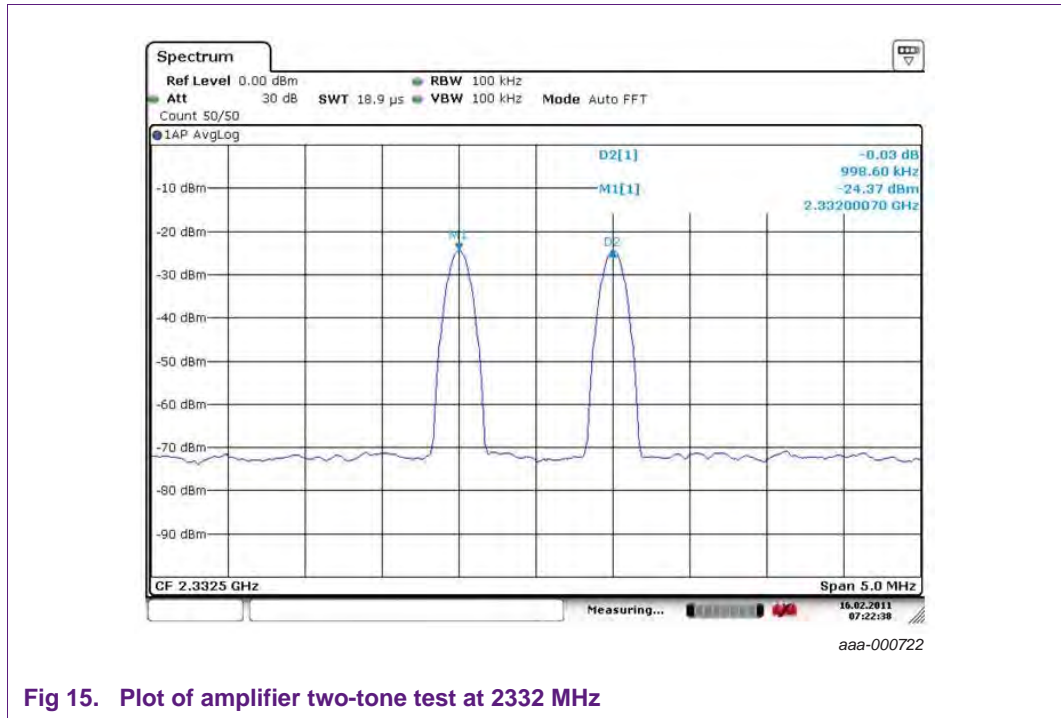


Fig 15. Plot of amplifier two-tone test at 2332 MHz



6.6.2 LNA response to two-tone test

- Output IP3 = 22.625 dBm
- Input IP3 = 22.625 dBm – (24.37 – 6.46) dBm = 4.7 dBm

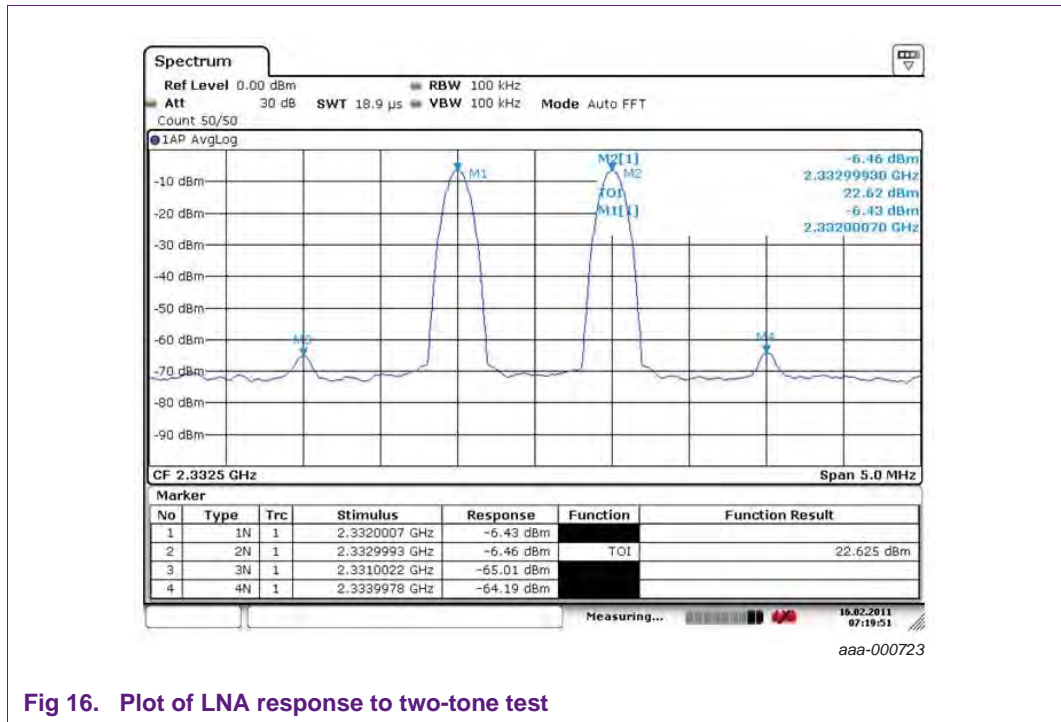


Fig 16. Plot of LNA response to two-tone test

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