PCB Layout Guidelines for PQFN/QFN Style Packages Requiring Thermal Vias for Heat Dissipation

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PURPOSE

This document provides guidelines for printed circuit board (PCB) designs for Power Quad Flat No-Lead (PQFN/QFN) packages soldered on thermal via. RF power devices typically generate heat that must be conducted away from the device. The heat source is on the die, and the die is located on the die flag or exposed heat spreader. To dissipate this heat through the PCB, the exposed heat spreader is attached to a center pad with via holes. The center pad is surrounded by peripheral pads that correspond to the peripheral leads of the device. The specific guidelines explained here are for RF power devices with PQFN and QFN packages (e.g., Case Outline Nos. 1894, 1543, 1898, etc.). These devices require an extensive thermal via structure in the PCB center pad area for thermal management. Figure 1 shows a typical PCB layout for this type of package showing via holes in the center pad as well as six peripheral pads, each on all four sides of the center pad. Figure 2 shows a typical cross-section of an RF Power device in a PQFN package surface mounted on the PCB. Freescale Application Note AN2467 for Power Quad Flat No-Lead (PQFN) packages provides necessary guidelines for designing the PCB layout for a typical PQFN package. The application note also covers reliability test results for solder joints when the guidelines are followed. This application note provides supplemental information to AN2467, and includes special requirements for devices that require thermal vias in the center pad.

Figure 1. Typical PCB Layout for 8x8 PQFN-24 Package

Figure 2. Typical Cross-section of PQFN Package for RF Power Device Surface Mounted on a PCB
BACKGROUND

Because of cost, the general trend for surface mount devices (SMD) with via holes in the solder pad is to have unfilled thermal via holes in the PCB. However, during solder reflow, the liquid solder tends to wick into the thermal via holes, resulting in solder volume loss between the exposed heat spreader and center pad. When the solder solidifies, the package is likely to be pulled down due to the large area of the center pad which will cause the extra solder under the peripheral leads of the package to spread out, forming so-called solder balls (see Figures 3 and 4). The solder-ball ing phenomenon has been well-known to occur during solder reflow of PQFN/QFN-type leadless packages, especially for center solder pads with extensive via holes. For fine-pitch components, the solder-ball ing phenomena can also result in solder bridging between two adjacent peripheral pads.

The solder-ball ing phenomenon generally does not present a reliability issue, but customers may be concerned that the solder balls can become loose during transport, installation, or operation and possibly create a short on the PCB trace. The design guidelines presented here are intended to minimize or eliminate this.

Many factors during the PQFN package solder reflow process affect solder balling, e.g., PCB layout, solder paste screen-printing thickness, aperture size, solder alloy and solder paste types, etc. For typical leaded SMT packages, the extra solder volume under the leads tends to wet on the front and back sides of the leads and create a fillet instead of forming solder balls at the end of the leads or bridging between leads. PQFN and QFN packages are leadless so they contain no lead against which a fillet can be formed to take away excess solder. However, the peripheral PCB pads can be designed to accommodate any excess solder under the peripheral leads, thus eliminating or reducing the probability of solder-ball ing and bridging phenomena.

PCB PAD LAYOUT RECOMMENDATIONS

The PCB pad layout includes the design of both the center pad and peripheral pads.

Recommendations from Application Note AN2467

Recommendations for peripheral pads from AN2467:
• Extension of the pad from the edge of the package (d) = 0.15 mm
• Width of the pad to be larger than lead nominal width on each side (e) by 0.025 mm
• Minimum distance between two adjacent pads = 0.15 mm
• Inside edge of the peripheral pad to be in line with inside edge of the peripheral lead and between 0.15 and 0.25 mm away from the center pad

Because AN2467 does not provide much information on the presence of via holes in the center pad and because concerns of solder balling, additional experiments were performed to define the minimum required values of pad dimension “d” to address these concerns. Dimension “d” is important for determining the pad extension needed to accommodate the excessive solder during solder reflow. Based on an internal evaluation using an 8x8 24-lead PQFN package, PCB pad layout guidelines are provided for customers to facilitate the design of the PCBs. These recommendations are provided as a guide and may require some refinement for a specific application or process. They are applicable for use with both Sn-Pb eutectic and Pb-free solder alloys.

Figure 3. Solder Balling During Solder Reflow to the PCB of PQFN Package

Figure 4. Typical Cross-section of PQFN Package Surface Mounted on PCB

The solder-ball ing phenomenon generally does not present a reliability issue, but customers may be concerned that the solder balls can become loose during transport, installation, or operation and possibly create a short on the PCB trace. The
BOARD MOUNTING EVALUATION

In general, the center pad with the thermal via should be the same size as the maximum dimension of the exposed heat spreader of the PQFN package. This helps the device to self-center and provides the maximum number of via holes in the pad. Another major consideration is the via pattern. The via holes should be designed to minimize the thermal resistance of the PCB. Before determining the via hole design, an analysis of the PCB assembly stack should be conducted to determine whether the device can operate within the acceptable limits for junction temperature and whether the PCB and the solder joint temperatures are within the acceptable limits for the materials selected.

A Design of Experiment (DOE) was conducted with dimension "d" as one of the parameters. In addition, the solder joint material (Sn-Pb-Ag or Sn62, as well as Pb-free solder alloy SAC305) was included as one of the parameters. Two different stencil thicknesses for solder paste printing were also used in the DOE. The full matrix is shown in Table 1.

Sample size in the DOE was five units per cell. The daisy chain test board was designed for 8x8 PQFN-24 package surface mount evaluation (see Figure 6). There was no die in the test unit. The peripheral leads of the package were internally connected (see Figure 7) by pad to pad wire bonds. After the packages were surface mounted on the test boards, six peripheral leads on each side were connected in series. Each side of the PQFN package surface mounted on the test board forms a separate loop with all of the solder joints on that side forming series resistors (see Figure 8).

PCB parameters:
- via drill diameter = 12 mils, or 0.30 mm
- via pitch = 24 mils, or 0.60 mm
- copper plating in the via ~1 mil, or ~0.025 mm
- PCB thickness = 59 mils, or 1.50 mm
- PCB material = FR4

Table 1. Evaluation Matrix for Design of Experiment on the Pad Extension

<table>
<thead>
<tr>
<th>Case #1</th>
<th>Stencil Thickness (mil)</th>
<th>Solder Alloy</th>
<th>Dimension “d” (mm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>4L-A</td>
<td>4</td>
<td>Sn62</td>
<td>0.00</td>
</tr>
<tr>
<td>4L-B</td>
<td>4</td>
<td>Sn62</td>
<td>0.20</td>
</tr>
<tr>
<td>4L-C</td>
<td>4</td>
<td>Sn62</td>
<td>0.40</td>
</tr>
<tr>
<td>4L-D</td>
<td>4</td>
<td>Sn62</td>
<td>0.60</td>
</tr>
<tr>
<td>4L-E</td>
<td>4</td>
<td>Sn62</td>
<td>0.80</td>
</tr>
<tr>
<td>6L-A</td>
<td>6</td>
<td>Sn62</td>
<td>0.00</td>
</tr>
<tr>
<td>6L-B</td>
<td>6</td>
<td>Sn62</td>
<td>0.20</td>
</tr>
<tr>
<td>6L-C</td>
<td>6</td>
<td>Sn62</td>
<td>0.40</td>
</tr>
<tr>
<td>6L-D</td>
<td>6</td>
<td>Sn62</td>
<td>0.60</td>
</tr>
<tr>
<td>6L-E</td>
<td>6</td>
<td>Sn62</td>
<td>0.80</td>
</tr>
<tr>
<td>4UL-A</td>
<td>4</td>
<td>SAC305</td>
<td>0.00</td>
</tr>
<tr>
<td>4UL-B</td>
<td>4</td>
<td>SAC305</td>
<td>0.20</td>
</tr>
<tr>
<td>4UL-C</td>
<td>4</td>
<td>SAC305</td>
<td>0.40</td>
</tr>
<tr>
<td>4UL-D</td>
<td>4</td>
<td>SAC305</td>
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<td>4UL-E</td>
<td>4</td>
<td>SAC305</td>
<td>0.80</td>
</tr>
<tr>
<td>6UL-A</td>
<td>6</td>
<td>SAC305</td>
<td>0.00</td>
</tr>
<tr>
<td>6UL-B</td>
<td>6</td>
<td>SAC305</td>
<td>0.20</td>
</tr>
<tr>
<td>6UL-C</td>
<td>6</td>
<td>SAC305</td>
<td>0.40</td>
</tr>
<tr>
<td>6UL-D</td>
<td>6</td>
<td>SAC305</td>
<td>0.60</td>
</tr>
<tr>
<td>6UL-E</td>
<td>6</td>
<td>SAC305</td>
<td>0.80</td>
</tr>
</tbody>
</table>
Figure 6. Daisy Chain Test Board for 8x8 PQFN-24 Package Solder Joint Evaluation

Figure 7. Internal Wire Bonds on Peripheral Leads (1.5 mil Au Wire) for Test Unit
Assembly Reflow

Solder paste was screen-printed on the PCB with two different thickness stencils (4 mils and 6 mils) and two different solder pastes (Sn62 and SAC305). The devices were picked and placed on top of the PCB pattern. The PCBs were then reflowed in a 10-zone convection belt furnace in air environment. The PCBs with Sn62 solder were reflowed using a peak temperature of 218°C; the PCBs with SAC305 (Pb-free) were reflowed using a peak reflow temperature of 242°C. After the reflow and cleaning step, the solder joints were examined by X-ray and visual inspection.

Solder Joints Visual and X-Ray Inspection

After the reflow, the solder joints were visually inspected first. For cases with d < 0.20 mm, solder balling was visible on most of the units evaluated. A typical case for Sn62 alloys is shown in Figure 9. The solder-balling phenomenon for Pb-free SAC305 solder is even more pronounced than that for Sn62 solder (Figure 10). For cases with d > 0.40 mm, no solder balling was observed for either solder material. Typical solder joints are shown in Figure 11 (for Sn62 alloy) and Figure 12 (for Pb-free SAC305 alloy).
Reliability Testing

After reviewing the DOE results, the case with $d = 0.4$ mm was chosen for a confirmation run with both Sn62 and Pb-free SAC305 solder alloys. The confirmation run used 25 units for each of the two cases. Again, the solder joints were visually inspected. The results were satisfactory as expected.

The test boards with daisy chain solder joints were then placed in a thermal cycling test. The temperature range for the thermal cycling test was from -40°C to 125°C with 15-minute dwell times at each extreme temperature. The duration of the test was 2,000 cycles. Electrical resistance measurements for each side of each test unit showed no solder joint failure. Figure 13 shows the comparison of solder joint resistance of the 50 thermal cycled boards with four non-thermal cycled boards shown as zero cycle data. The electrical resistance measurement revealed that there was no increase in the solder joint resistance. Also on visual examination, no sign of solder joint cracking was observed in either Sn62 or SAC305 solder alloy samples.
PAD LAYOUT RECOMMENDATIONS

Based on these evaluation results, Freescale recommends using the following guidelines to determine the pad layout for PQFN/QFN-style packages that require a large number of via holes in the center pad:

1. Create symmetry of the leads and pads so that the device can self-center on the pad layout.
2. Design the center pad so that it is equivalent to maximum value of the exposed pad on the PQFN/QFN package.
3. Specify that the width of the peripheral pad is at least 0.05 mm larger than the nominal dimension of peripheral leads.
4. Keep the inside edge of the peripheral pad to be in line with the inside edge of the peripheral leads at the maximum dimension.
5. Allow sufficient distance between the peripheral pads (0.15 mm minimum recommended) to accommodate the solder mask. This will prevent shorting between two pads or between two leads.
6. Allow sufficient distance between the center pad and the inside edge of the peripheral pads (0.15 mm minimum recommended) to accommodate the solder mask and prevent shorting between the center pad and peripheral leads or between the peripheral pads or leads.
7. Specify that the peripheral pad extension past the package (dimension “d” in Figure 5) is at least 40% of the peripheral lead length nominal dimension.

These recommendations are provided as a guide. In some instances compromises may have to be considered between conflicting requirements.

Some PQFN style packages also have peripheral pads in four corners of the package (e.g. Case 1543). The recommendations given here for the peripheral pad layout are also applicable to the corner pad layout.

The pad layout for the 8x8 PQFN-24 package (Case 1894) using these guidelines is shown to create a solder joint free of solder bailing. This solder joint is also shown to survive the normal reliability requirements of a typical RF power device.

The complete pad layout for the 8x8 PQFN-24 (Case 1894) device using these guidelines is shown in Appendix A as Figure A-1. Based on the guidelines derived from experiments with 8x8 PQFN-24 (Case 1894), the pad layouts for 5x5 PQFN-16 (Case 1543) and 4x4 QFN-16 (Case 1898) packages used for RF Power devices are shown in Figure A-2 and Figure A-3 respectively. As more products move into this style of leadless packages, new guidelines will be added.

References

Freescale Application Note AN2467, Power Quad Flat Pack No-Lead (PQFN).
Appendix A

Figure A-1. PCB Pads Layout for 8x8 PQFN-24 (Case 1894)

Figure A-2. PCB Pad Layout for 5x5 PQFN-16 (Case 1543)

Figure A-3. PCB Pad Layout for 4x4 QFN-16 (Case 1898)